Advanced Computer Graphics Materials 1

Matthias Teschner

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Outline

- Context
- Bidirectional Reflectance Distribution Function BRDF
 - Definition
 - Application
 - Exemplary materials
 - Properties
- Reflectance
- Material modeling
- Transparent materials

Context



- Light absorption and scattering at surfaces is governed by material properties
- How to represent material properties?

Surface Reflection Properties

 How much incident light from a particular direction is reflected into a particular direction?
 ⇒ Bidirectional Reflectance Distribution Function BRDF f_r



Surface Reflection Models

- Surfaces have reflection properties
 - How much flux is absorbed?
 - Which part of the flux is reflected?
 - How is it reflected?
- E.g., empirical Phong model
 - Efficient to compute
 - Physically motivated
 - Does not capture all aspects of real materials (too few degrees of freedom)

Surface Reflection Models

- Theoretical reflectance models
 - Have more degrees of freedom
- Theoretical models can consider
 - Incoming and outgoing angle of flux
 - Incoming and outgoing wavelength of flux (fluorescence)
 - Incoming and outgoing polarization (linear and circular)
 - Incoming and outgoing position (subsurface scattering)
 - Time delay between incoming and outgoing flux (phosphorescence)

Surface Reflection Models

- Incident light is partially reflected or absorbed depending on the absorbance spectrum of the surface (surface color)
- Reflected light is scattered by the surface depending on the surface roughness
 - Smooth surface (small patches with uniform orientation)
 - Specular or glossy reflection
 - Light is reflected into dominant reflection directions
 - Rough surface (small patches with varying orientation)
 - Diffuse (Lambertian) reflection
 - Light is reflected into many directions



Can be described by relating incident and exitant flux



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Materials



diffuse

glossy

transparent

subsurface scattering

[Oliver Wetter]

[David Turesson]

[https://cgiknowledge.wordpress.com/]



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Introduction

- Incident radiance $L_i(\boldsymbol{p}, \boldsymbol{\omega}_i)$ at position \boldsymbol{p} from direction $-\boldsymbol{\omega}_i$ induces irradiance at \boldsymbol{p} : $dE_i(\boldsymbol{p}, \boldsymbol{\omega}_i) = L_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \cos \theta_i d\omega_i$
- Flux is partially absorbed: $\int_{\text{coefficient.}}^{0 \le p \le 1 \text{ is a}} dB_i(\boldsymbol{p}, \boldsymbol{\omega}_i) = \rho(\boldsymbol{p}) dE_i(\boldsymbol{p}, \boldsymbol{\omega}_i)$
- Reflected flux into direction $\boldsymbol{\omega}_o$ $\mathrm{d}L_o(\boldsymbol{p}, \boldsymbol{\omega}_o) \sim \mathrm{d}B_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \sim \mathrm{d}E_i(\boldsymbol{p}, \boldsymbol{\omega}_i)$



 ω_i represents the direction of the incident radiance. Per definition, all directions point away from the surface. I.e., incident radiance travels along $-\omega_i$.

Reflection pattern Reflectance

Definition

- For all pairs of directions ω_i and ω_o , the ratio of outgoing radiance towards ω_o and irradiance due to incoming radiance from $-\omega_i$ is referred to as BRDF: $f_r(\boldsymbol{p}, \omega_i, \omega_o) = \frac{\mathrm{d}L_o(\boldsymbol{p}, \omega_o)}{\mathrm{d}E_i(\boldsymbol{p}, \omega_i)}$
- BRDF typically depends on a position and two directions
 - Directions form a solid angle of 2π for opaque surfaces and 4π for transparent surfaces
 - Various variants. E.g., BRDF can depend on two positions for subsurface scattering $f_r(\boldsymbol{p}_i, \boldsymbol{p}_o, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\mathrm{d}L_o(\boldsymbol{p}_o, \boldsymbol{\omega}_o)}{\mathrm{d}E_i(\boldsymbol{p}_i, \boldsymbol{\omega}_i)}$

Application

- Relation between irradiance and exitant radiance $dL_o(\mathbf{p}, \boldsymbol{\omega}_o) = f_r(\mathbf{p}, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) dE_i(\mathbf{p}, \boldsymbol{\omega}_i)$
- Irradiance is induced by radiance $dL_o(\boldsymbol{p}, \boldsymbol{\omega}_o) = f_r(\boldsymbol{p}, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) L_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \cos \theta_i d\omega_i$
- Integration over the hemisphere \Rightarrow reflectance equation $L_o(\mathbf{p}, \boldsymbol{\omega}_o) = \int_{2\pi} f_r(\mathbf{p}, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) L_i(\mathbf{p}, \boldsymbol{\omega}_i) \cos \theta_i d\omega_i$
- Reflectance equation establishes a relation between incident and exitant radiance

Reflectance Equation



 $L_o(\boldsymbol{p}, \boldsymbol{\omega}_o) = \int_{2\pi} f_r(\boldsymbol{p}, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) L_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \cos \theta_i d\omega_i$

 $L_o(\boldsymbol{p}, \boldsymbol{\omega}_o) \approx \sum_i f_r(\boldsymbol{p}, \boldsymbol{\omega}_i, \boldsymbol{\omega}_o) L_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \cos \theta_i \Delta \omega_i$

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Reflectance Equation



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Example - Diffuse Reflection

Lambertian model

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 Def: Reflected flux is proportional to the cosine of the angle between flux direction and surface normal

$$= \Phi \sim \cos \theta
= \Phi^{\perp} = \frac{\Phi_1}{\cos \theta_1} = \frac{\Phi_2}{\cos \theta_2}
= Outgoing radiance is equal in all directions
$$L_1 = \frac{d^2 \Phi_1}{d\omega_1 \cdot \cos \theta_1 \cdot dA} = d\omega_2 \text{ denote two solid angles of the same size with different directions.}}$$$$

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Example - Diffuse Reflection

- From a viewer's perspective
 - More flux per surface area is sent towards viewer 1

$$\Phi^{\perp} = \frac{\Phi_1}{\cos \theta_1} = \frac{\Phi_2}{\cos \theta_2} = \frac{\Phi_i}{\cos \theta_i}$$

- Viewer 2 receives flux from (sees) a larger surface area $A^{\perp} = A_1 \cdot \cos \theta_1 = A_2 \cdot \cos \theta_2 = A_i \cdot \cos \theta_i$
- Both effects cancel which results in the same flux and radiance towards both viewers





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BRDF for Diffuse Reflecting Material

- Illumination $L_i(\boldsymbol{\omega}_i)$
- Induced surface irradiance $dE_i(\boldsymbol{\omega}_i) = L_i(\boldsymbol{\omega}_i) \cdot \cos \theta_i \cdot d\omega_i$
- Overall irradiance $E = \int_{2\pi} L_i(\boldsymbol{\omega}_i) \cdot \cos \theta_i \cdot d\omega_i$
- Partially absorbed. Resulting radiosity

$$B=
ho\cdot E$$
 $0\leq
ho\leq 1$ ho - reflectance

$$B = \int_{2\pi} L_o(\boldsymbol{\omega}_o) \cdot \cos \theta_o \cdot \mathrm{d}\omega_o = L_o \cdot \int_{2\pi} \cos \theta_o \mathrm{d}\omega_o = L_o \cdot \pi \quad \text{see next slide}$$

$$\rho \cdot E = \pi \cdot L_o \quad L_o = \frac{\rho}{\pi} E = \int_{2\pi} \frac{\rho}{\pi} \cdot L_i(\boldsymbol{\omega}_i) \cdot \cos \theta_i \cdot d\omega_i$$

 $\Rightarrow f_{r,d}(oldsymbol{\omega}_i,oldsymbol{\omega}_o) = rac{
ho}{\pi}~$ BRDF is constant for diffuse reflecting material

Integrating Over Solid Angles

- Directions can be represented with two angles
- Differential area spanning from θ to θ +d θ and from ϕ to ϕ +d ϕ $dA = r d\theta r \sin \theta d\phi$ see next slide
- Differential solid angle $d\omega = \frac{dA}{r^2} = \sin\theta \ d\theta \ d\phi$
- E.g., integral over the hemisphere
 - $\int_{2\pi} f(\boldsymbol{\omega}) \, \mathrm{d}\boldsymbol{\omega} = \int_{0}^{2\pi} \int_{0}^{\frac{\pi}{2}} f(\theta, \phi) \sin\theta \, \mathrm{d}\theta \, \mathrm{d}\phi$



 2π indicates the hemisphere above an opaque surface

Integrating Over Solid Angles



Exemplary Integrals

- Solid angle of a hemisphere $\int_{2\pi} 1 d\omega = \int_0^{2\pi} \int_0^{\frac{\pi}{2}} \sin \theta \, d\theta \, d\phi = \int_0^{2\pi} \left[-\cos \theta \right]_0^{\frac{\pi}{2}} \, d\phi$ $= \int_0^{2\pi} 1 \, d\phi$

$$=2\pi$$

– Solid angle of a sphere

$$\int_{4\pi} 1 d\omega = \int_0^{2\pi} \int_0^{\pi} \sin \theta \, d\theta \, d\phi = \int_0^{2\pi} \left[-\cos \theta \right]_0^{\pi} \, d\phi$$
$$= \int_0^{2\pi} 2 \, d\phi$$
$$= 4\pi$$

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Integrating a Cosine Lobe

- E.g., to determine the irradiance at a point
 - $E_i(\mathbf{p}) = \int_{2\pi} L_i(\mathbf{p}, \boldsymbol{\omega}_i) \cos \theta_i \mathrm{d}\omega_i$
- General form

$$\int_0^{2\pi} \int_0^{\frac{\pi}{2}} \cos^n \theta \sin \theta \, \mathrm{d}\theta \, \mathrm{d}\phi = \int_0^{2\pi} \left[-\frac{\cos^{n+1} \theta}{n+1} \right]_0^{\frac{\pi}{2}} \, \mathrm{d}\phi = \int_0^{2\pi} \frac{1}{n+1} \, \mathrm{d}\phi = \frac{2\pi}{n+1}$$

- E.g., constant radiance from / into all directions $E(\boldsymbol{p}) = \int_{2\pi} L_i(\boldsymbol{p}, \boldsymbol{\omega}_i) \cos \theta_i d\omega_i = L_i(\boldsymbol{p}) \int_{2\pi} \cos \theta_i d\omega_i = \pi L_i(\boldsymbol{p})$ $B(\boldsymbol{p}) = \int_{2\pi} L_o(\boldsymbol{p}, \boldsymbol{\omega}_o) \cos \theta_o d\omega_o = L_o(\boldsymbol{p}) \int_{2\pi} \cos \theta_o d\omega_o = \pi L_o(\boldsymbol{p})$ Difference fluctions
- Diffuse reflection $L_o(\mathbf{p}) = \frac{B(\mathbf{p})}{\pi} = \frac{\rho}{\pi} E(\mathbf{p})$

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Example – Mirror Reflection

- Each ray of incident flux produces one ray of outgoing flux into a mirrored direction
- Reflectance $0 \le \rho \le 1$
- BRDF

$$f_{r,m}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \rho \, \frac{1}{\cos \theta_i \sin \theta_i} \, \delta(\theta_o - \theta_i) \, \delta(\phi_o \pm \pi - \phi_i)$$



Example – Mirror Reflection

- Delta function $x \neq 0 \rightarrow \delta(x) = 0$ $\int \delta(x) dx = 1$ $\int f(x)\delta(y-x) dx = f(y)$ $\int f(x)\delta(x-y) dx = f(y)$



- Mirrored radiance $L_{o}(\theta_{o}, \phi_{o}) = \int_{0}^{2\pi} \int_{0}^{\frac{\pi}{2}} \rho \frac{1}{\cos \theta_{i} \sin \theta_{i}} \delta(\theta_{o} - \theta_{i}) \delta(\phi_{o} \pm \pi - \phi_{i}) L_{i}(\theta_{i}, \phi_{i}) \cos \theta_{i} \sin \theta_{i} d\theta_{i} d\phi_{i}$ $= \rho \int_{0}^{2\pi} \delta(\phi_{o} \pm \pi - \phi_{i}) \int_{0}^{\frac{\pi}{2}} L_{i}(\theta_{i}, \phi_{i}) \delta(\theta_{o} - \theta_{i}) d\theta_{i} d\phi_{i}$ $= \rho \int_{0}^{2\pi} L_{i}(\theta_{o}, \phi_{i}) \delta(\phi_{o} \pm \pi - \phi_{i}) d\phi_{i}$ $= \rho L_{i}(\theta_{o}, \phi_{o} \pm \pi) = \rho L_{i}(\theta_{i}, \phi_{i})$ University of Freiburg - Computer Science Department - 26

- Values are positive $f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \geq 0$
 - Incident flux cannot induce negative exitant flux
- Helmholtz reciprocity: $f_r(\boldsymbol{\omega}_o, \boldsymbol{\omega}_i) = f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o)$
 - If incident and exitant flux are reversed, the BRDF value remains the same

- Values can be arbitrarily large

- E.g., mirror reflection
- Ratio of exitant flux to the illumination effect of incident flux

$$f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\mathrm{d}L_o(\boldsymbol{\omega}_o)}{\mathrm{d}E_i(\boldsymbol{\omega}_i)} = \frac{\mathrm{d}L_o(\boldsymbol{\omega}_o)}{L_i(\boldsymbol{\omega}_i)\cos\theta_i\mathrm{d}\omega_i}$$
 Graphs are shown for one specific, fixed ω_i





 If the solid angle of reflected flux gets smaller, the respective BRDF values get larger

Example - Glossy / Specular Reflection

- Incoming flux from direction ω_i is scattered, but concentrated around the reflection direction ω_o
- Reflectance $0 \le \rho \le 1$
- BRDF

 $f_{r,s}(oldsymbol{\omega}_i,oldsymbol{\omega}_o) =$

$$\rho ((2(\boldsymbol{n} \cdot \boldsymbol{\omega}_i) \cdot \boldsymbol{n} - \boldsymbol{\omega}_i) \cdot \boldsymbol{\omega}_o)^e$$

In this term, n, ω_i , ω_o are represented with 3D normalized vectors



 $L_i(\boldsymbol{\omega}_i)$

Example - Glossy / Specular Reflection

- BRDF
$$f_{r,s}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) =
ho \; ((2(\boldsymbol{n} \cdot \boldsymbol{\omega}_i) \cdot \boldsymbol{n} - \boldsymbol{\omega}_i) \cdot \boldsymbol{\omega}_o)^e$$
 in ω_i, ω_o are represented with 3D normalized vectors

- $r(n, \omega_i) = 2(n \cdot \omega_i) \cdot n - \omega_i$ is the reflection direction of ω_i

- α is the angle between $r(n, \omega_i)$ and ω_o



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- Linearity
 - If a material is defined as a combination of BRDFs, the contributions of the BRDFs are added for the total outgoing radiance



Exitant radiance for incident radiance from ω_i for a combined material (diffuse + specular, f_{r,d} + f_{r,s})

[Suffern]

Example – Mixed Diffuse / Specular Reflection

- Weighted average of diffuse and specular reflection

$$f_{r,ds}(\boldsymbol{\omega}_i,\boldsymbol{\omega}_o) = \alpha \, \frac{\rho_d}{\pi} + \beta \, \rho_s \, \left((2(\boldsymbol{n} \cdot \boldsymbol{\omega}_i) \cdot \boldsymbol{n} - \boldsymbol{\omega}_i) \cdot \boldsymbol{\omega}_o \right)^e$$

- Relation to Phong illumination model
 - Normalized light source direction \boldsymbol{l} , viewer \boldsymbol{v} , normal \boldsymbol{n} $L_o^{\mathrm{P}}(\boldsymbol{v}) = \frac{\rho_d}{\pi} L_i(\boldsymbol{l}) \ \boldsymbol{n} \cdot \boldsymbol{l} + \rho_s \ L_i(\boldsymbol{l}) \ \boldsymbol{n} \cdot \boldsymbol{l} \ (\boldsymbol{r} \cdot \boldsymbol{v})^e$
 - Reflection equation

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$$L_o^{\mathrm{R}}(\boldsymbol{v}) = \int_{2\pi} f_r(\boldsymbol{\omega}_i, \boldsymbol{v}) L_i(\boldsymbol{\omega}_i) \cos \theta_i \mathrm{d}\omega_i$$
$$\approx f_r(\boldsymbol{l}, \boldsymbol{v}) L_i(\boldsymbol{l}) \ \boldsymbol{n} \cdot \boldsymbol{l} \ \Delta \omega_i$$
$$f_r(\boldsymbol{l}, \boldsymbol{w}) = \int_{2\pi}^{\rho_d} d_{\boldsymbol{\omega}_i} \int_{2\pi}^{\rho_s} (\boldsymbol{n}, \boldsymbol{w})^e \to L^{\mathrm{P}}(\boldsymbol{w}) = \boldsymbol{L}$$

$$E_r(\boldsymbol{l}, \boldsymbol{v}) = rac{
ho_d}{\pi \cdot \Delta \omega} + rac{
ho_s}{\Delta \omega} (\boldsymbol{r} \cdot \boldsymbol{v})^e \Rightarrow L_o^{\mathrm{P}}(\boldsymbol{v}) = L_o^{\mathrm{R}}(\boldsymbol{v})$$

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BRDF Properties - Energy Conservation

Eric Veach: Robust Monte Carlo Methods for Light Transport Simulation, Ph.D. dissertation, Stanford University, 1997.

- Incident radiance / illumination from direction $\omega_i = (\theta_i, \phi_i)$ $L_i(\theta, \phi) = \frac{1}{\sin \theta_i \cos \theta_i} \delta(\theta - \theta_i) \delta(\phi - \phi_i)$
- Irradiance
 - $E = \int \int L_i(\theta, \phi) \cos \theta \sin \theta \, \mathrm{d}\theta \, \mathrm{d}\phi = 1$
- Exitant radiance in direction $\omega_o = (\theta_o, \phi_o)$ $L_o(\theta_o, \phi_o) = \int \int L_i(\theta, \phi) f_r(\theta, \phi, \theta_o, \phi_o) \cos \theta \sin \theta \, d\theta \, d\phi = f_r(\theta_i, \phi_i, \theta_o, \phi_o)$ - Radiosity

 $B = \int \int L_o(\theta_o, \phi_0) \cos \theta_o \sin \theta_o \, d\theta_o \, d\phi_o = \int \int f_r(\theta_i, \phi_i, \theta_o, \phi_o) \cos \theta_o \, \sin \theta_o \, d\theta_o \, d\phi_o$ $B \le E \Rightarrow \int \int f_r(\theta_i, \phi_i, \theta_o, \phi_o) \, \cos \theta_o \, \sin \theta_o \, d\theta_o \, d\phi_o \le 1$ $\forall \boldsymbol{\omega}_i : \int_{2\pi} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \, \cos \theta_o \, d\omega_o \le 1$

BRDF Summary - Properties

- Definition: $f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\mathrm{d}L_o(\boldsymbol{\omega}_o)}{\mathrm{d}E_i(\boldsymbol{\omega}_i)} = \frac{\mathrm{d}L_o(\boldsymbol{\omega}_o)}{L_i(\boldsymbol{\omega}_i)\cdot\cos\theta_i\cdot\mathrm{d}\omega_i}$
- Positive: $f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \geq 0$
- Helmholtz reciprocity: $f_r(\boldsymbol{\omega}_o, \boldsymbol{\omega}_i) = f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o)$
 - Incident and exitant radiance can be reversed
- Energy conservation: $\forall \boldsymbol{\omega}_i : \int_{2\pi} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \cos \theta_o \mathrm{d} \boldsymbol{\omega}_o \leq 1$
- Linearity
 - If a material is defined as a sum of BRDFs, the contributions of the BRDFs are added for the total outgoing radiance $\int (f_{r,1} + f_{r,2})L_i \cos \theta_i d\omega_i = \int f_{r,1}L_i \cos \theta_i d\omega_i + \int f_{r,2}L_i \cos \theta_i d\omega_i$

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BRDF Summary – Exemplary Materials

– Diffuse

$$f_{r,d}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = rac{
ho}{\pi}$$

– Mirror

$$f_{r,m}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \rho \, \frac{1}{\cos \theta_i \sin \theta_i} \, \delta(\theta_o - \theta_i) \, \delta(\phi_o \pm \pi - \phi_i)$$

– Specular

$$f_{r,s}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) =
ho \; ((2(\boldsymbol{n} \cdot \boldsymbol{\omega}_i) \cdot \boldsymbol{n} - \omega_i) \cdot \boldsymbol{\omega}_o)^e \quad \stackrel{\text{n, } \omega_i, \ \omega_o}{\text{with 3D normalized vectors}}$$

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Reflectance

- Ratio of outgoing flux to incident flux
 - Surface property, used in BRDFs
- Incident flux $d\Phi_i = dA \int_{\Omega_i} L_i(\boldsymbol{\omega}_i) \cos \theta_i d\omega_i$ $(E = \frac{d\Phi}{dA} = \int_{\Omega_i} L_i \cos \theta_i d\omega_i)$
- Outgoing flux $d\Phi_o = dA \int_{\Omega_o} L_o(\boldsymbol{\omega}_o) \cos \theta_o d\omega_o$

 $d\Phi_o = dA \int_{\Omega_o} \int_{\Omega_i} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) L_i(\boldsymbol{\omega}_i) \cos \theta_i \cos \theta_o d\omega_i d\omega_o$

- Reflectance $\rho(\Omega_i, \Omega_o) = \frac{\mathrm{d}\Phi_o}{\mathrm{d}\Phi_i} = \frac{\mathrm{d}A\int_{\Omega_o} L_o(\boldsymbol{\omega}_o)\cos\theta_o\mathrm{d}\omega_o}{\mathrm{d}A\int_{\Omega_i} L_i(\boldsymbol{\omega}_i)\cos\theta_i\mathrm{d}\omega_i} = \frac{\mathrm{d}A\int_{\Omega_o}\int_{\Omega_i} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o)L_i(\boldsymbol{\omega}_i)\cos\theta_i\mathrm{d}\omega_i\mathrm{d}\omega_o}{\mathrm{d}A\int_{\Omega_i} L_i(\boldsymbol{\omega}_i)\cos\theta_i\mathrm{d}\omega_i}$

– Various parameterizations of the reflectance can be considered for various configurations of Ω_i, Ω_o

Bihemispherical Reflectance

Diffuse material

$$\begin{split} \rho(2\pi, 2\pi) &= \frac{\mathrm{d}\Phi_o}{\mathrm{d}\Phi_i} = \frac{\mathrm{d}A \int_{2\pi} L_o(\boldsymbol{\omega}_o) \cos \theta_o \mathrm{d}\omega_o}{\mathrm{d}A \int_{2\pi} L_i(\boldsymbol{\omega}_i) \cos \theta_i \mathrm{d}\omega_i} \\ &= \frac{\mathrm{d}L_o \int_{2\pi} \cos \theta_o \mathrm{d}\omega_o}{\mathrm{d}E(\boldsymbol{\omega}_i)} \quad \text{Exitant radiance is equal in all direction} \\ &= \pi \frac{\mathrm{d}L_o}{\mathrm{d}E(\boldsymbol{\omega}_i)} \\ &= \pi f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \quad \text{BRDF definition} \end{split}$$

- The reflectance in the BRDF for diffuse material is a bihemispherical reflectance $f_r(\omega_i, \omega_o) = \frac{\rho(2\pi, 2\pi)}{\pi}$
- The ratio of exitant and incident flux is independent from the directions of incident and exitant flux

Spectral Bihemispherical Reflectance

- Spectral reflectance is wavelength dependent $\rho_{\lambda}(\Omega_i, \Omega_o) = \frac{\mathrm{d}\Phi_{o,\lambda}}{\mathrm{d}\Phi_{i,\lambda}}$
- Diffuse spectral reflectance (spectrum represented with RGB values) $\rho_{red} = \pi \frac{dL_{o,red}}{dE_{red}} \rho_{green} = \pi \frac{dL_{o,green}}{dE_{green}} \rho_{blue} = \pi \frac{dL_{o,blue}}{dE_{blue}}$ RGB surface color - Diffuse spectral BRDF

$$f_{r,d,\mathrm{red}}(\boldsymbol{\omega}_i,\boldsymbol{\omega}_o) = \frac{\rho_{\mathrm{red}}}{\pi} f_{r,d,\mathrm{green}}(\boldsymbol{\omega}_i,\boldsymbol{\omega}_o) = \frac{\rho_{\mathrm{green}}}{\pi} f_{r,d,\mathrm{blue}}(\boldsymbol{\omega}_i,\boldsymbol{\omega}_o) = \frac{\rho_{\mathrm{blue}}}{\pi}$$

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Bidirectional Reflectance

 How much of the flux from an incident direction is reflected into an exitant direction $L_i(\boldsymbol{\omega}_i) = \frac{\mathrm{d}^2 \Phi_i}{\mathrm{d} A \cos \theta_i \, \mathrm{d} \omega_i} \Rightarrow \mathrm{d}^2 \Phi_i = \mathrm{d} A \, L_i(\boldsymbol{\omega}_i) \, \cos \theta_i \, \mathrm{d} \omega_i$ $dL_o(\boldsymbol{\omega}_o) = f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \ L_i(\boldsymbol{\omega}_i) \cos \theta_i d\omega_i = \frac{d^3 \Phi_o}{dA \cos \theta_o d\omega_o}$ $\Rightarrow d^{3}\Phi_{o} = f_{r}(\boldsymbol{\omega}_{i}, \boldsymbol{\omega}_{o}) \ L_{i}(\boldsymbol{\omega}_{i}) \cos \theta_{i} d\omega_{i} dA \ \cos \theta_{o} \ d\omega_{o}$ $d\rho(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{d^3 \Phi_o}{d^2 \Phi_i} = \frac{f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \ L_i(\boldsymbol{\omega}_i) \cos \theta_i d\omega_i dA \ \cos \theta_o \ d\omega_o}{dA \ L_i(\boldsymbol{\omega}_i) \ \cos \theta_i \ d\omega_i}$ $d\rho(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \cos \theta_o d\omega_o$ Dependent on incident and exitant flux directions

Directional-Hemispherical Reflectance

$$d\rho(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \cos \theta_o d\omega_o$$
$$\rho(\boldsymbol{\omega}_i, 2\pi) = \int_{2\pi} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \cos \theta_o d\omega_o$$

- The term $0 \leq \int_{2\pi} f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \cos \theta_o d\omega_o \leq 1$ represents the ratio of exitant flux into the hemisphere and incident flux from direction ω_i
- Another intuition for the energy conservation constraint of a BRDF

Material Reflectances

- Diffuse, mirror, specular $f_{r,d}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\rho_d}{\pi}$ $f_{r,m}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \rho_m \frac{1}{\cos \theta_i \sin \theta_i} \, \delta(\theta_o - \theta_i) \, \delta(\phi_o \pm \pi - \phi_i)$ $f_{r,s}(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \rho_s \, \left((2(\boldsymbol{n} \cdot \boldsymbol{\omega}_i) \cdot \boldsymbol{n} - \boldsymbol{\omega}_i) \cdot \boldsymbol{\omega}_o \right)^e \qquad \stackrel{\text{n, } \boldsymbol{\omega}_i, \, \boldsymbol{\omega}_o \text{ are represented}}{\text{with 3D normalized vectors}}$
- In a diffuse BRDF, ρ_d accounts for diffuse reflectance, i.e. the surface color. In glossy, specular, mirror BRDFs, ρ_m, ρ_s is typically (1,1,1), i.e. white. The color of specular highlights converges towards the color of the light source.

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Microfacet Model

- Light scattering at a surface is determined by the distribution of microfacets
- Facets reflect perfectly specular or perfectly diffuse
- Distribution of microfacet normals governs material



n_f n

[Pharr, Humphreys]

Rough surface Large variation of facet normals Smooth surface Small variation of facet normals

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Diffuse Reflecting Material

- Facets are perfectly diffuse
- Flux into a detector element is an aggregate value over many facets
- Due to local facet effects, the radiance is not perfectly Lambertian, but potentially view-dependent



Surface

[Wikipedia: Oren-Nayar reflectance model]

Local Facet Effects

- Masking
 - Microfacet is not visible to the viewer
- Shadowing
 - Microfacet is not illuminated
- Interreflection
 - Microfacets illuminate each other (additional illumination)



[Pharr, Humphreys]

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Oren-Nayar Diffuse Material

- Models rough opaque diffuse surfaces
- Facets are Lambertian, symmetric V-shaped grooves
- Gaussian distribution models the facet normals
- Parameter $0 \leq \sigma^2 \leq 1$ gives the variance of the angle between surface normal and facet normal
- viewer direction $\boldsymbol{\omega}_o = (\theta_o, \phi_o)$, light direction $\boldsymbol{\omega}_i = (\theta_i, \phi_i)$
- BRDF $f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\rho_d}{\pi} (A + B \max(0, \cos(\phi_i \phi_o)) \sin \alpha \tan \beta)$

$$A = 1 - \frac{\sigma^2}{2(\sigma^2 + 0.33)} \quad B = \frac{0.45\sigma^2}{\sigma^2 + 0.09} \quad \alpha = \max(\theta_i, \theta_o) \quad \beta = \min(\theta_i, \theta_o)$$

Oren-Nayar Diffuse Reflectance



[Wikipedia: Oren-Nayar reflectance model]

- Comparisons [Oren, Nayar, ACM SIGGRAPH 1994]



Oren-Nayar

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Oren-Nayar vs. Lambertian

- Is brighter for large angles between viewer and surface normal compared to a Lambertian surface
- Gets brighter if the angle between viewer and light gets smaller
- Converges to a Lambertian surface $f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{\rho_d}{\pi} (A + B \max(0, \cos(\phi_i - \phi_o)) \sin \alpha \tan \beta)$ $A = 1 - \frac{\sigma^2}{2(\sigma^2 + 0.33)} \quad B = \frac{0.45\sigma^2}{\sigma^2 + 0.09}$
- If all facets have the same normal, then $\sigma = 0$, A = 1, B = 0: $f_r(\omega_i, \omega_o) = \frac{\rho_d}{\pi}$

Oren-Nayar - View Dependence

- Different combinations of projected areas of dark and bright facets for different viewer directions
- Maximal brightness, if viewing direction corresponds to light direction



[Srinivasa Narasimhan http://www.cs.cmu.edu/afs/cs/academic/class/16823-f06/]

Torrance-Sparrow Specular Material

- Models rough opaque specular surfaces
- Facets are perfect mirrors, symmetric and V-shaped
- Beckmann distribution models the facet normals
- Similar models: Cook-Torrance, Blinn
- Viewer direction $\omega_o = (\theta_o, \phi_o)$
- Light source $\boldsymbol{\omega}_i = (\theta_i, \phi_i)$
- Halfway direction $\boldsymbol{\omega}_h(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o)$

- BRDF
$$f_r(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) = \frac{D(\boldsymbol{\omega}_h) \ G(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o) \ F(\boldsymbol{\omega}_o)}{\pi \ \cos \theta_i \ \cos \theta_o}$$
 D - Beckmann distribution
G - geometric term for sha

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shadowing

Beckmann Distribution

- Describes the roughness of the surface
- *m* describes the roughness
- β is the angle between halfway vector and surface normal



Geometric Term / Fresnel Term

– Geometric term

- Accounts for self-shadowing effects of microfacets
- Fresnel term
 - Accounts for a varying absorbance / reflection ratio depending on the angle of incident flux (direction dependent reflectance)
 - Many surfaces reflect more strongly if illumination is nearly parallel to the surface

Outline

- Context
- Bidirectional Reflectance Distribution Function BRDF
 - Definition
 - Application
 - Exemplary materials
 - Properties
- Reflectance
- Material modeling
- Transparent materials

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- Light is reflected and refracted at the interface between two transparent media
- Incident, reflected, and transmitted rays are in the same plane
- Direction t is determined by ω_o and by the indices of refraction η_{out} and η_{in}



[Suffern]

Snell's Law

– Materials are characterized by a refractive index

- Ratio of the speed of light in vacuum and in the considered medium
- Vacuum 1.0, air 1.0003, ice 1.31, water 1.33, glass 1.5
- Snell's law / law of refraction
 - $\frac{\sin \theta_i}{\sin \theta_t} = \frac{\eta_{in}}{\eta_{out}} = \eta \quad \text{Relative refraction index}$
- Transmission direction

$$- t = \frac{1}{\eta} \boldsymbol{\omega}_o - (\cos \theta_t - \frac{1}{\eta} \cos \theta_i) \boldsymbol{n}_i$$

- $\cos \theta_t = (1 \frac{1}{\eta^2} (1 \cos^2 \theta_i))^{\frac{1}{2}}$
- All vectors should be normalized, then t is also normalized

Snell's Law

– For η >1, transmitted rays are bent towards the normal

– For η <1, transmitted rays are bent away from the normal





[Suffern]

Total Internal Reflection

- For η <1 and $\theta_i > \theta_c$ (critical angle), total internal reflection occurs
- Transmitted ray is bent towards the interface until the incident light ray reaches the critical angle

- For
$$\theta_i = \theta_c$$
: $1 - \frac{1}{\eta^2}(1 - \cos^2 \theta_i) = 0$

- For $\theta_i > \theta_c$: $1 - \frac{1}{\eta^2}(1 - \cos^2 \theta_i) < 0$



Reflectance Equation

- Incident, BRDF weighted radiance is integrated over the hemisphere to compute the outgoing radiance $L_o(\omega_o) = \int_{2\pi} f_r(\omega_i, \omega_o) L_i(\omega_i) \cos \theta_i d\omega_i$
- Can also consider transmitted light
- BTDF bidirectional transmittance distribution function
 - $-f_t(\boldsymbol{\omega}_i, \boldsymbol{\omega}_o)$ with $\boldsymbol{\omega}_i$ and $\boldsymbol{\omega}_o$ in opposite hemispheres
- BRDF and BTDF can be combined to a BSDF bidirectional scattering distribution function $L_o(\omega_o) = \int_{4\pi} f(\omega_i, \omega_o) L_i(\omega_i) |\cos \theta_i| d\omega_i$

Specular Transmission

- Snell's law gives the direction of a refracted ray and its radiance change
- Motivation
 - Solid angle of a differential cone of incident radiance changes due to refraction
- $L_t = \rho_t \frac{\eta_t^2}{\eta_i^2} L_i$ with $0 \le \rho_t \le 1$ being the transmission coefficient





[Suffern]

Specular Transmission

- Ray and radiance-transfer direction
- At point *a*, radiance transfer is from inside to outside

 $\eta_i = \eta_{in} \quad \eta_t = \eta_{out}$

At point *b*, radiance transfer is from outside to inside

$$\eta_i = \eta_{out} \ \eta_t = \eta_{in}$$

Radiance changes cancel when a ray enters and leaves a medium

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[Suffern]

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Reflectance and Transmittance

- Fresnel equations describe which fractions of incident light are reflected and transmitted
- Fractions depend on the refraction indices and on the incident light direction
- Fresnel reflectance $F_r = \frac{1}{2} \left(\left(\frac{\eta \cos \theta_i \cos \theta_t}{\eta \cos \theta_i + \cos \theta_t} \right)^2 + \left(\frac{\cos \theta_i \eta \cos \theta_t}{\cos \theta_i + \eta \cos \theta_t} \right)^2 \right)$

- Fresnel transmittance $F_t = 1 - F_r$

Reflectance and Transmittance

- General form

$$F_{r} = \frac{1}{2} \left(\left(\frac{\eta \cos \theta_{i} - \cos \theta_{t}}{\eta \cos \theta_{i} + \cos \theta_{t}} \right)^{2} + \left(\frac{\cos \theta_{i} - \eta \cos \theta_{t}}{\cos \theta_{i} + \eta \cos \theta_{t}} \right)^{2} \right)$$
- Normal incidence $\theta_{i} = \theta_{t} = 0$

$$F_{r} = \frac{1}{2} \left(\left(\frac{\eta - 1}{\eta + 1} \right)^{2} + \left(\frac{1 - \eta}{1 + \eta} \right)^{2} \right)$$

- E.g., $F_r = 0.04$ at the interface of air and glass with $\eta = 1.5$
- Grazing incidence $\theta_i = \frac{\pi}{2}$ $F_r = 1$

Reflectance and Transmittance

 Reflectance and transmittance of glass for varying incident angles



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Light Attenuation

- Transparent materials attenuate light
 - Light is scattered / absorbed along the ray
 - Radiance decreases exponentially with distance
 - Beer-Lambert law
 - Transparent materials are examples of participating media

Light Attenuation

$$-L_a = c_f^d L_b$$

- -d is the distance inside a medium
- $-L_{a}$ is exitant radiance, L_{b} is incident radiance
- c describes the attenuation (wavelength-dependent)
 - c = (1, 1, 1) no attenuation
 - -c = (1,1,0.9) blue is attenuated, resulting in a yellow appearance

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Light Attenuation

– Examples





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