Simulation in Computer Graphics Grid Fluids

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Motivation



$$rac{\mathrm{d}\boldsymbol{v}}{\mathrm{d}t} = \boldsymbol{g} +
u
abla^2 \boldsymbol{v} - rac{1}{
ho}
abla p$$

Lagrangian: Acceleration of a moving parcel.



Eulerian: Acceleration at a static cell.

 $\frac{\mathrm{D}\boldsymbol{v}}{\mathrm{D}t} = \boldsymbol{g} + \nu \nabla^2 \boldsymbol{v} - \frac{1}{\rho} \nabla p$

$$\frac{\mathbf{D}\boldsymbol{v}}{\mathbf{D}t} = \frac{\partial\boldsymbol{v}}{\partial t} + (\boldsymbol{v}\cdot\nabla)\boldsymbol{v} \quad \text{or}$$
$$\frac{\mathbf{D}\boldsymbol{v}}{\mathbf{D}t} = \frac{\mathrm{d}\boldsymbol{v}}{\mathrm{d}t} \quad \frac{\mathrm{d}\boldsymbol{x}}{\mathrm{d}t} = \boldsymbol{v}$$

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Grid-based Fluids

- Benefits
 - Fixed neighbor sets
 - Constant sampling quality
 - Accuracy
- Challenges

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- Free surfaces
- Complex boundaries
- Moving boundaries

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[Lorenzo Rossini]

Grid-based Fluids



[Enright et al., SIGGRAPH 2002]

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Outline

- Particles vs. grids
- Advection of the velocity field
- Simple grid fluid solvers
- Discussion

Fluid Solvers

- Fluid solvers compute velocity fields that represent the fluid flow
- The velocity field is sampled at discrete time points t and discrete positions x_i



Velocity field at time t

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- Particles
 - Are small fractions of the fluid body
 - Represent some volume
 - Have a mass according to volume and density
 - Position moves with the flow
 - Velocity represents the velocity of the fluid parcel



$$\frac{\mathrm{d}\boldsymbol{x}_i(t)}{\mathrm{d}t} = \boldsymbol{v}_i(t)$$

- Grid cells
 - Contain small fractions of the fluid body
 - Represent some volume
 - Contain some mass according to volume and density
 - Position is static
 - Velocity represents the flow velocity through the cell container



$$\frac{\mathrm{d}\boldsymbol{x}_i(t)}{\mathrm{d}t} = 0$$

- Both concepts compute the same velocity field, but typically at different sample positions
- Grid solvers do not move the samples with the flow
- Particle solvers
 move the samples
 with the flow



– Particles

- Velocity updates $v_i(t + \Delta t) = v_i(t) + \Delta t \frac{dv_i(t)}{dt}$ at a particle *i* are computed using the Navier-Stokes equation

$$\frac{\mathrm{d}\boldsymbol{v}_i(t)}{\mathrm{d}t} = -\frac{1}{\rho_i(t)}\nabla p_i(t) + \nu\nabla^2 \boldsymbol{v}_i(t) + \boldsymbol{g} = \boldsymbol{a}_i(t)$$

- $\frac{d\boldsymbol{v}_i(t)}{dt}$ is the time rate of change of a particle, i.e. sample that is advected with the flow: $\boldsymbol{x}_i(t + \Delta t) = \boldsymbol{x}_i(t) + \Delta t \boldsymbol{v}_i(t)$
- Advection of the samples accounts for the advection of the flow

– Grid samples

- Velocity updates $v_i(t + \Delta t) = v_i(t) + \Delta t \frac{\partial v_i(t)}{\partial t}$ at a grid cell *i* are computed using the Navier-Stokes equation $\frac{\partial v_i(t)}{\partial t} = a_i(t) - (v_i(t) \cdot \nabla)v_i(t)$
- $\frac{\partial v_i(t)}{\partial t}$ is the time rate of change of a static sample with $x_i(t + \Delta t) = x_i(t)$
- $-(\boldsymbol{v}_i(t) \cdot \nabla) \boldsymbol{v}_i(t)$ accounts for the advection of the flow



– Grid samples



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Particles vs. Grids – 1D Illustration

Particle approach $v_j(t + \Delta t) = v_i(t) + \Delta t a_i(t)$ Grid approach $v_i(t + \Delta t) = v_i(t) + \Delta t (a_i(t) - (v_i(t) \cdot \nabla) v_i(t))$



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Particles vs. Grids – 1D Illustration

- Navier-Stokes
 - Time rate of change of the velocity of an advected position $\frac{\mathrm{d}v_i(t)}{\mathrm{d}t} = a_i(t)$
 - Time rate of change of the velocity at a fixed position $\frac{\partial v_i(t)}{\partial t} = a_i(t) - (v_i(t) \cdot \nabla) v_i(t)$

Particles vs. Grids – 1D Illustration

– Relation

- Two sample positions $x_1(t_1), x_2(t_2)$ with $x_2(t_2) = x_1(t_1) + \Delta t v(x_1, t_1)$

Notation

$$v(x_i, t_i) = v_i(t_i)$$

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Taylor approximation of the velocity

$$v(x_{2},t_{2}) = v(x_{1},t_{1}) + \frac{\partial v(x_{1},t_{1})}{\partial x}(x_{2}-x_{1}) + \frac{\partial v(x_{1},t_{1})}{\partial t}(t_{2}-t_{1})$$

$$\frac{v(x_{2},t_{2})-v(x_{1},t_{1})}{\Delta t} = \frac{\partial v(x_{1},t_{1})}{\partial x}\frac{(x_{2}-x_{1})}{\Delta t} + \frac{\partial v(x_{1},t_{1})}{\partial t}\frac{(t_{2}-t_{1})}{\Delta t}$$

$$\frac{v(x_{2},t_{2})-v(x_{1},t_{1})}{\Delta t} = \frac{\partial v(x_{1},t_{1})}{\partial x}v(x_{1},t_{1}) + \frac{\partial v(x_{1},t_{1})}{\partial t}$$

$$\frac{dv(x_{1},t_{1})}{dt} = \frac{\partial v(x_{1},t_{1})}{\partial t} + (v(x_{1},t_{1})\cdot\nabla)v(x_{1},t_{1})$$

$$\frac{dv}{dt} = \frac{\partial v}{\partial t} + (v\cdot\nabla)v$$

Material Derivative

 $- \frac{D\boldsymbol{v}_{i}(t)}{Dt} = \frac{d\boldsymbol{v}_{i}(t)}{dt} = \frac{\partial \boldsymbol{v}_{i}(t)}{\partial t} + (\boldsymbol{v}_{i}(t) \cdot \nabla)\boldsymbol{v}_{i}(t) \text{ is the time rate of change of the velocity of a moving fluid element}$ $- \frac{D\boldsymbol{v}_{i}(t)}{Dt} = \frac{d\boldsymbol{v}_{i}(t)}{dt} \text{ if } i \text{ is a moving particle with } \frac{d\boldsymbol{x}_{i}(t)}{dt} = \boldsymbol{v}_{i}(t)$ $- \frac{D\boldsymbol{v}_{i}(t)}{Dt} = \frac{\partial \boldsymbol{v}_{i}(t)}{\partial t} + (\boldsymbol{v}_{i}(t) \cdot \nabla)\boldsymbol{v}_{i}(t) \text{ if } i \text{ is a static grid cell}$ $- \frac{D\boldsymbol{v}_{i}(t)}{Dt} = -\frac{1}{\rho_{i}(t)}\nabla p_{i}(t) + \nu\nabla^{2}\boldsymbol{v}_{i}(t) + \boldsymbol{g}$

- Is a general form of the Navier-Stokes equation
- *i* can be a particle or a grid cell
- Particle techniques are referred to as Lagrangian
- Grid techniques are referred to as Eulerian

Navier-Stokes on Grids

$$- \frac{\mathrm{D}\boldsymbol{v}_i(t)}{\mathrm{D}t} = \frac{\partial\boldsymbol{v}_i(t)}{\partial t} + (\boldsymbol{v}_i(t)\cdot\nabla)\boldsymbol{v}_i(t) = -\frac{1}{\rho_i(t)}\nabla p_i(t) + \nu\nabla^2\boldsymbol{v}_i(t) + \boldsymbol{g}$$

- Grid approaches often work with per-volume quantities in contrast to per-mass quantities - $\rho_i(t) \left(\frac{\partial \boldsymbol{v}_i(t)}{\partial t} + (\boldsymbol{v}_i(t) \cdot \nabla) \boldsymbol{v}_i(t) \right) = -\nabla p_i(t) + \mu \nabla^2 \boldsymbol{v}_i(t) + \rho_i(t) \boldsymbol{g}$
- $\frac{\partial v_i(t)}{\partial t} + (v_i(t) \cdot \nabla) v_i(t)$ is the time rate of change of the velocity of a moving fluid element
- $-\frac{\partial \boldsymbol{v}_i(t)}{\partial t}$ is the local acceleration
- $(\mathbf{v}_i(t) \cdot \nabla)\mathbf{v}_i(t)$ is the convective acceleration

Grid-based Fluid Solvers

- Grid solvers compute $\frac{\partial v_i(t)}{\partial t}$ at all grid cells
- Velocities at grid cells are updated with, e.g., $v_i(t+\Delta t) = v_i(t) + \Delta t \frac{\partial v_i(t)}{\partial t} = v_i(t) + \Delta t \left(-\frac{1}{\rho_i(t)} \nabla p_i(t) + \nu \nabla^2 v_i(t) + g - (v_i(t) \cdot \nabla) v_i(t) \right)$
- Spatial derivatives can be approximated with, e.g., finite differences in 1D $\nabla p_i(t) = \frac{p(x_i + \Delta x, t) - p(x_i - \Delta x, t)}{2\Delta x}$ with Δx being the grid cell size

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Overview

- Navier-Stokes: $\frac{\partial \boldsymbol{v}(\boldsymbol{x}_i,t)}{\partial t} = -\frac{1}{\rho(\boldsymbol{x}_i,t)} \nabla p(\boldsymbol{x}_i,t) + \nu \nabla^2 \boldsymbol{v}(\boldsymbol{x}_i,t) + \boldsymbol{g} (\boldsymbol{v}(\boldsymbol{x}_i,t) \cdot \nabla) \boldsymbol{v}(\boldsymbol{x}_i,t)$
- Advection equation: $\frac{\partial \boldsymbol{v}(\boldsymbol{x}_i,t)}{\partial t} = -(\boldsymbol{v}(\boldsymbol{x}_i,t)\cdot\nabla)\boldsymbol{v}(\boldsymbol{x}_i,t)$
 - Velocity $\boldsymbol{v}(\boldsymbol{x}_i,t)$ is advected by velocity $\boldsymbol{v}(\boldsymbol{x}_i,t)$
- 1D advection equation: $\frac{\partial T(x_i,t_i)}{\partial t} = -(v \cdot \nabla)T(x_i,t_i) = -v \frac{\partial T(x_i,t_i)}{\partial x}$

– Temperature T advected by constant velocity v

- Computation of $T(x_i, t_i + \Delta t)$ with $T(x_i, t_i + \Delta t) = T(x_i, t_i) + \Delta t \frac{\partial T(x_i, t_i)}{\partial t} = T(x_i, t_i) - \Delta t v \frac{\partial T(x_i, t_i)}{\partial x}$ - Discretization of $\frac{\partial T(x_i, t_i)}{\partial x}$ with finite differences

1D Advection of a 1D Quantity

– E.g., 1D temperature field is advected by 1D velocity / wind



- $T(x_i, t_0)$ is known at all positions x_i at time t_0

Advection

- How to compute $T(x_i, t_i)$ at arbitrary positions x_i and times t_i ?



- Analytic solution $T(x_i, t_i) = T(x_i v \cdot (t_i t_0), t_0)$
- $T(x_i, t_i)$ is obtained by shifting x_i through a distance $v \cdot (t_i t_0)$ without changing the shape of T

Advection on a Grid – 1D

- Discretize time and space: $t_{i+1} - t_i = \Delta t$ $x_{i+1} - x_i = \Delta x$



- T is considered at discrete positions and time points

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Advection on a Grid

- How to compute $T(x_i, t_{i+1})$ from $T(x_i, t_i)$?
- If T is linear: $T(x_{i+1}, t_i)$ $\uparrow T$ $\frac{T(x_i, t_i) - T(x_i, t_{i+1})}{v\Delta t} = \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x}$ $T(x_i, t_i)$ $T(x_{i-1}, t_i)$ $\frac{T(x_i, t_{i+1}) - T(x_i, t_i)}{\Delta t} = -v \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x}$ wind speed v 1D advection equation $T(x_i, t_{i+1})$ $x_i - \Delta x \ x_i \quad x_i + \Delta x$ \mathcal{X}

$$\frac{\partial T(x_i, t_i)}{\partial t} = -v \frac{\partial T(x_i, t_i)}{\partial x}$$

1D Advection Equation on a Grid

- The continuous form $\frac{\partial T(x_i,t_i)}{\partial t} = -v \frac{\partial T(x_i,t_i)}{\partial x}$ is discretized $- \text{E.g.,} \quad \frac{T(x_i, t_{i+1}) - T(x_i, t_i)}{\Delta t} = -v \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x}$ central difference forward difference - This equation contains only one unknown $T(x_i, t_{i+1})$ $-T(x_i, t_{i+1}) = T(x_i, t_i) - \Delta t v \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x}$ $-T(x_i, t_{i+1}) = T(x_i, t_i) + \Delta t \frac{\partial T(x_i, t_i)}{\partial t} = T(x_i, t_i) - \Delta t v \frac{\partial T(x_i, t_i)}{\partial x}$ - If $T(x_i, t_i)$ is known at all samples, i.e. grid cells x_i , at time t_i , $T(x_i, t_{i+1})$ at the next time t_{i+1} can be computed at all grid cells x_i

Finite Differences

- The time derivative is commonly discretized as $\frac{\partial T(x_i,t_i)}{\partial t} = \frac{T(x_i,t_{i+1}) - T(x_i,t_i)}{\Delta t} + O(\Delta t)$ - The spatial derivative is discretized in various ways $\frac{\partial T(x_i,t_i)}{\partial x} = \frac{T(x_{i+1},t_i) - T(x_i,t_i)}{\Delta x} + O(\Delta x) \quad \text{forward difference}$ $\frac{\partial T(x_i,t_i)}{\partial x} = \frac{T(x_i,t_i) - T(x_{i-1},t_i)}{\Delta x} + O(\Delta x) \quad \text{backward difference}$ $\frac{\partial T(x_i,t_i)}{\partial x} = \frac{T(x_{i+1},t_i) - T(x_{i-1},t_i)}{2\Delta x} + O(\Delta x^2) \quad \text{central difference}$

Solving the 1D Advection Equation

- Upwind (v > 0)

 $\frac{T(x_i,t_{i+1})-T(x_i,t_i)}{\Delta t} = -v\frac{T(x_i,t_i)-T(x_{i-1},t_i)}{\Delta x} \qquad T(x_i,t_{i+1}) = T(x_i,t_i) - v\Delta t\frac{T(x_i,t_i)-T(x_{i-1},t_i)}{\Delta x}$ - Downwind (v > 0)

 $\frac{T(x_i, t_{i+1}) - T(x_i, t_i)}{\Delta t} = -v \frac{T(x_{i+1}, t_i) - T(x_i, t_i)}{\Delta x} \qquad T(x_i, t_{i+1}) = T(x_i, t_i) - v \Delta t \frac{T(x_{i+1}, t_i) - T(x_i, t_i)}{\Delta x}$

Centered (forward time centered space FTCS)

 $\frac{T(x_{i},t_{i+1})-T(x_{i},t_{i})}{\Delta t} = -v\frac{T(x_{i+1},t_{i})-T(x_{i-1},t_{i})}{2\Delta x} \qquad T(x_{i},t_{i+1}) = T(x_{i},t_{i}) - v\Delta t\frac{T(x_{i+1},t_{i})-T(x_{i-1},t_{i})}{2\Delta x}$ - Leap-frog

$$\frac{T(x_i,t_{i+1})-T(x_i,t_{i-1})}{2\Delta t} = -v\frac{T(x_{i+1},t_i)-T(x_{i-1},t_i)}{2\Delta x} \quad T(x_i,t_{i+1}) = T(x_i,t_{i-1}) - v\Delta t\frac{T(x_{i+1},t_i)-T(x_{i-1},t_i)}{\Delta x}$$

Solving the 1D Advection Equation

Lax-Wendroff

 $T(x_i, t_{i+1}) = T(x_i, t_i) - v\Delta t \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x} + \frac{1}{2}v^2\Delta t^2 \frac{T(x_{i+1}, t_i) - 2T(x_i, t_i) + T(x_{i-1}, t_i)}{\Delta x^2}$

– Beam-Warming

 $T(x_i, t_{i+1}) = T(x_i, t_i) - v\Delta t \frac{3T(x_i, t_i) - 4T(x_{i-1}, t_i) + T(x_{i-2}, t_i)}{2\Delta x} + \frac{1}{2}v^2\Delta t^2 \frac{T(x_i, t_i) - 2T(x_{i-1}, t_i) + T(x_{i-2}, t_i)}{\Delta x^2}$

Lax-Friedrichs

 $T(x_i, t_{i+1}) = \frac{1}{2} \left(T(x_{i-1}, t_i) + T(x_{i+1}, t_i) \right) - v \Delta t \frac{T(x_{i+1}, t_i) - T(x_{i-1}, t_i)}{2\Delta x}$

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Finite Differences

- Are one way to approximate spatial derivatives for grid cells
 Can be used to, e.g., compute the pressure gradient
- in the Navier-Stokes equation at grid cells
- Can also approximate higher-order derivatives, e.g. $\frac{\partial^2 T(x_i,t_i)}{\partial x^2} = \frac{T(x_{i+1},t_i)-2T(x_i,t_i)+T(x_{i-1},t_i)}{\Delta x^2} + O(\Delta x^2)$
- Can also compute more accurate approximations $\frac{\partial T(x_i,t_i)}{\partial x} = \frac{T(x_{i-2},t_i) - 8T(x_{i-1},t_i) + 8T(x_{i+1},t_i) - T(x_{i+2},t_i)}{\Delta x^2} + O(\Delta x^4)$ $\frac{\partial^2 T(x_i,t_i)}{\partial x^2} = \frac{-T(x_{i-2},t_i) + 16T(x_{i-1},t_i) - 30T(x_i,t_i) + 16T(x_{i+1},t_i) - T(x_{i+2},t_i)}{\Delta x^2} + O(\Delta x^4)$

3D Advection Equation on a Grid

- $1D \text{ form:} \qquad \frac{\partial T(x_i, t_i)}{\partial t} = -v \frac{\partial T(x_i, t_i)}{\partial x} \\ \text{ General form:} \qquad \frac{\partial T(x_i, t_i)}{\partial t} = -v \nabla T(x_i, t_i) \qquad \text{grid cell position and} \\ \text{velocity are vectors} \\ \text{ In 3D:} \qquad \frac{\partial T(x_i, t_i)}{\partial t} = -v \left(\begin{array}{c} \frac{\partial T(x_i, t_i)}{\partial x_i} \\ \frac{\partial T(x_i, t_i)}{\partial y_i} \\ \frac{\partial T(x_i, t_i)}{\partial z_i} \end{array} \right) = -(v \cdot \nabla)T(x_i, t_i)$
- Advecting a vector quantity $T: \frac{\partial T(\boldsymbol{x}_i, t_i)}{\partial t} = -(\boldsymbol{v} \cdot \nabla)T(\boldsymbol{x}_i, t_i)$
- In the Eulerian form of the Navier-Stokes equation, the velocity at a position is advected by the velocity at that position $\frac{\partial \boldsymbol{v}(\boldsymbol{x}_i,t_i)}{\partial t} = -(\boldsymbol{v}(\boldsymbol{x}_i,t_i)\cdot\nabla)\boldsymbol{v}(\boldsymbol{x}_i,t_i)$

Advecting the Velocity Field

$$\frac{\partial \boldsymbol{v}(\boldsymbol{x}_{i},t_{i})}{\partial t} = -(\boldsymbol{v}(\boldsymbol{x}_{i},t_{i}) \cdot \nabla) \boldsymbol{v}(\boldsymbol{x}_{i},t_{i})$$
speed $\boldsymbol{v}(\boldsymbol{x}_{i},t_{i})$
speed $\boldsymbol{v}(\boldsymbol{x}_{i},t_{i})$
speed $\boldsymbol{v}(\boldsymbol{x}_{j},t_{i})$
 $\boldsymbol{v}(\boldsymbol{x}_{j},t_{i})$
 $\boldsymbol{v}(\boldsymbol{x}_{j},t_{i})$
 \boldsymbol{x}_{i}
 \boldsymbol{x}_{j}
 \boldsymbol{x}_{j}

- Application in the Navier-Stokes equation $\frac{\partial \boldsymbol{v}(\boldsymbol{x}_i, t_i)}{\partial t} = -\frac{1}{\rho(\boldsymbol{x}_i, t_i))} \nabla p(\boldsymbol{x}_i, t_i) + \nu \nabla^2 \boldsymbol{v}(\boldsymbol{x}_i, t_i) + \boldsymbol{g} - (\boldsymbol{v}(\boldsymbol{x}_i, t_i) \cdot \nabla) \boldsymbol{v}(\boldsymbol{x}_i, t_i)$ University of Freiburg – Computer Science Department – 31

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1D/3D Velocity Advection on a Grid

$$- 1D: \frac{\partial v(x_i,t_i)}{\partial t_i} = -v(x_i,t_i)\frac{\partial v(x_i,t_i)}{\partial x_i} - 3D: \frac{\partial v(x_i,t_i)}{\partial t} = -(v(x_i,t_i)\cdot\nabla)v(x_i,t_i) = -\begin{pmatrix} v_x(x_i,t_i)\frac{\partial}{\partial x_x} & v_x(x_i,t_i)\frac{\partial}{\partial x_y} & v_x(x_i,t_i)\frac{\partial}{\partial x_z} \\ v_y(x_i,t_i)\frac{\partial}{\partial x_x} & v_y(x_i,t_i)\frac{\partial}{\partial x_y} & v_y(x_i,t_i)\frac{\partial}{\partial x_z} \\ v_z(x_i,t_i)\frac{\partial}{\partial x_x} & v_z(x_i,t_i)\frac{\partial}{\partial x_y} & v_z(x_i,t_i)\frac{\partial}{\partial x_z} \end{pmatrix} \begin{pmatrix} v_x(x_i,t_i) \\ v_y(x_i,t_i) \\ v_z(x_i,t_i) \end{pmatrix} = -\begin{pmatrix} v_x(x_i,t_i)\frac{\partial v_x}{\partial x_x}(x_i,t_i) + v_y(x_i,t_i)\frac{\partial v_x}{\partial x_y}(x_i,t_i) + v_z(x_i,t_i)\frac{\partial v_x}{\partial x_z}(x_i,t_i) \\ v_x(x_i,t_i)\frac{\partial v_x}{\partial x_x}(x_i,t_i) + v_y(x_i,t_i)\frac{\partial v_y}{\partial x_y}(x_i,t_i) + v_z(x_i,t_i)\frac{\partial v_z}{\partial x_z}(x_i,t_i) \end{pmatrix}$$

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Governing Equations in 2D

– Momentum equation at position (x_i, y_j) at time t

$$-\left(\frac{\partial \boldsymbol{v}}{\partial t}\right)_{i,j}^t = -\frac{1}{\rho_{i,j}^t} \nabla p_{i,j}^t - (\boldsymbol{v}_{i,j}^t \cdot \nabla) \boldsymbol{v}_{i,j}^t$$

- Inviscid flow (artificial viscosity)
- No body force, non-conservation form

- State equation
$$p_{i,j}^t = k(\frac{\rho_{i,j}^t}{\rho_0} - 1)$$

- Continuity equation at position (x_i, y_j) at time t

$$-\left(\frac{\partial\rho}{\partial t}\right)_{i,j}^{t} = -\rho_{i,j}^{t}\nabla\cdot\boldsymbol{v}_{i,j}^{t} - (\boldsymbol{v}_{i,j}^{t}\cdot\nabla)\rho_{i,j}^{t}$$

- Follows from
$$\frac{\mathrm{D}\rho}{\mathrm{D}t} = \frac{\partial\rho}{\partial t} + (\boldsymbol{v}\cdot\nabla)\rho$$

- Used for differential density update

Notation

$$\boldsymbol{v}_{i,j}^t = \boldsymbol{v}(x_i, y_j, t)$$

Governing Equations in 2D

$$\begin{split} \left(\frac{\partial \boldsymbol{v}}{\partial t}\right)_{i,j}^{t} &= -\frac{1}{\rho_{i,j}^{t}} \nabla p_{i,j}^{t} - (\boldsymbol{v}_{i,j}^{t} \cdot \nabla) \boldsymbol{v}_{i,j}^{t} \\ \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^{t} &= -\rho_{i,j}^{t} \nabla \cdot \boldsymbol{v}_{i,j}^{t} - (\boldsymbol{v}_{i,j}^{t} \cdot \nabla) \rho_{i,j}^{t} \\ \boldsymbol{v}_{i,j}^{t} &= (u_{i,j}^{t}, v_{i,j}^{t})^{\mathsf{T}} \\ \left(\frac{\partial u}{\partial t}\right)_{i,j}^{t} &= -\left(\frac{1}{\rho_{i,j}^{t}} \left(\frac{\partial p}{\partial x}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial u}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial u}{\partial y}\right)_{i,j}^{t}\right) \\ \left(\frac{\partial v}{\partial t}\right)_{i,j}^{t} &= -\left(\frac{1}{\rho_{i,j}^{t}} \left(\frac{\partial p}{\partial y}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial v}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial v}{\partial y}\right)_{i,j}^{t}\right) \\ \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^{t} &= -\left(\rho_{i,j}^{t} \left(\frac{\partial u}{\partial x}\right)_{i,j}^{t} + \rho_{i,j}^{t} \left(\frac{\partial v}{\partial y}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial \rho}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial \rho}{\partial y}\right)_{i,j}^{t}\right) \end{split}$$

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Solver Illustration



Simple 2D Grid Fluid Solver

 $\begin{aligned} & \text{for all cell } (i,j) \text{ do} \\ & p_{i,j}^t = k (\frac{\rho_{i,j}^t}{\rho_0} - 1) \end{aligned} \\ & \text{Pressure from density} \end{aligned} \\ & \text{for all cell } (i,j) \text{ do} \\ & \left(\frac{\partial u}{\partial t}\right)_{i,j}^t = - \left(\frac{1}{\rho_{i,j}^t} \left(\frac{\partial p}{\partial x}\right)_{i,j}^t + u_{i,j}^t \left(\frac{\partial u}{\partial x}\right)_{i,j}^t + v_{i,j}^t \left(\frac{\partial u}{\partial y}\right)_{i,j}^t\right) \end{aligned} \\ & \text{Velocity change per time} \\ & \left(\frac{\partial v}{\partial t}\right)_{i,j}^t = - \left(\frac{1}{\rho_{i,j}^t} \left(\frac{\partial p}{\partial y}\right)_{i,j}^t + u_{i,j}^t \left(\frac{\partial v}{\partial x}\right)_{i,j}^t + v_{i,j}^t \left(\frac{\partial v}{\partial y}\right)_{i,j}^t\right) \end{aligned} \\ & \text{Velocity change per time} \\ & \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^t = - \left(\rho_{i,j}^t \left(\frac{\partial u}{\partial x}\right)_{i,j}^t + \rho_{i,j}^t \left(\frac{\partial v}{\partial y}\right)_{i,j}^t + u_{i,j}^t \left(\frac{\partial \rho}{\partial x}\right)_{i,j}^t + v_{i,j}^t \left(\frac{\partial \rho}{\partial y}\right)_{i,j}^t\right) \end{aligned} \\ & \text{Density change per time} \end{aligned}$

Velocity update for a cell Velocity update for a cell Density update for a cell

for all cell i, j do

$$u_{i,j}^{t+\Delta t} = u_{i,j}^{t} + \Delta t \left(\frac{\partial u}{\partial t}\right)_{i,j}^{t}$$
$$v_{i,j}^{t+\Delta t} = v_{i,j}^{t} + \Delta t \left(\frac{\partial v}{\partial t}\right)_{i,j}^{t}$$
$$\rho_{i,j}^{t+\Delta t} = \rho_{i,j}^{t} + \Delta t \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^{t}$$

Simple 2D Grid Fluid Solver

- No neighbor search / fixed neighbor sets
- Pressure computation, e.g. state equation or PPE
- Spatial derivatives computed, e.g., with finite differences
 - Interestingly, SPH would also be an option
 - Pressure gradient and velocity divergence are also used in particle solvers
 - Advection terms only occur in grid solvers
- Velocity and density update per static cell
- No sample advection

Discretization with Finite Differences

The time derivatives

$$\begin{pmatrix} \frac{\partial u}{\partial t} \end{pmatrix}_{i,j}^{t} = -\left(\frac{1}{\rho_{i,j}^{t}} \left(\frac{\partial p}{\partial x}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial u}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial u}{\partial y}\right)_{i,j}^{t} \right)$$

$$\begin{pmatrix} \frac{\partial v}{\partial t} \end{pmatrix}_{i,j}^{t} = -\left(\frac{1}{\rho_{i,j}^{t}} \left(\frac{\partial p}{\partial y}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial v}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial v}{\partial y}\right)_{i,j}^{t} \right)$$

$$\begin{pmatrix} \frac{\partial \rho}{\partial t} \end{pmatrix}_{i,j}^{t} = -\left(\rho_{i,j}^{t} \left(\frac{\partial u}{\partial x}\right)_{i,j}^{t} + \rho_{i,j}^{t} \left(\frac{\partial v}{\partial y}\right)_{i,j}^{t} + u_{i,j}^{t} \left(\frac{\partial \rho}{\partial x}\right)_{i,j}^{t} + v_{i,j}^{t} \left(\frac{\partial \rho}{\partial y}\right)_{i,j}^{t} \right)$$
are expressed with spatial derivatives

are expressed with spatial derivatives $\left(\frac{\partial p}{\partial x}\right)_{i,j}^t, \left(\frac{\partial p}{\partial y}\right)_{i,j}^t, \left(\frac{\partial \rho}{\partial x}\right)_{i,j}^t, \left(\frac{\partial \rho}{\partial y}\right)_{i,j}^t, \left(\frac{\partial u}{\partial x}\right)_{i,j}^t, \left(\frac{\partial u}{\partial y}\right)_{i,j}^t, \left(\frac{\partial v}{\partial x}\right)_{i,j}^t, \left(\frac{\partial v}{\partial y}\right)_{i,j}^t$

Discretization with Finite Differences

– E.g., using second-order central differences

$$\begin{split} \left(\frac{\partial u}{\partial t}\right)_{i,j}^{t} &= -\left(\frac{1}{\rho_{i,j}^{t}}\frac{p_{i+1,j}^{t}-p_{i-1,j}^{t}}{2\Delta x} + u_{i,j}^{t}\frac{u_{i+1,j}^{t}-u_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t}\frac{u_{i,j+1}^{t}-u_{i,j-1}^{t}}{2\Delta y}\right) \\ \left(\frac{\partial v}{\partial t}\right)_{i,j}^{t} &= -\left(\frac{1}{\rho_{i,j}^{t}}\frac{p_{i,j+1}^{t}-p_{i,j-1}^{t}}{2\Delta y} + u_{i,j}^{t}\frac{v_{i+1,j}^{t}-v_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t}\frac{v_{i,j+1}^{t}-v_{i,j-1}^{t}}{2\Delta y}\right) \\ \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^{t} &= -\left(\rho_{i,j}^{t}\frac{u_{i+1,j}^{t}-u_{i-1,j}^{t}}{2\Delta x} + \rho_{i,j}^{t}\frac{v_{i,j+1}^{t}-v_{i,j-1}^{t}}{2\Delta y} + u_{i,j}^{t}\frac{v_{i,j+1}^{t}-v_{i,j-1}^{t}}{2\Delta y}\right) \\ &+ u_{i,j}^{t}\frac{\rho_{i+1,j}^{t}-\rho_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t}\frac{\rho_{i,j+1}^{t}-\rho_{i,j-1}^{t}}{2\Delta y}\right) \end{split}$$

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Lax-Wendroff Technique

- Velocity and density update with $u_{i,j}^{t+\Delta t} = u_{i,j}^t + \Delta t \left(\frac{\partial u}{\partial t}\right)_{i,j}^t + \frac{\Delta t^2}{2} \left(\frac{\partial^2 u}{\partial t^2}\right)_{i,j}^t$

$$v_{i,j}^{t+\Delta t} = v_{i,j}^t + \Delta t \left(\frac{\partial v}{\partial t}\right)_{i,j}^t + \frac{\Delta t^2}{2} \left(\frac{\partial^2 v}{\partial t^2}\right)_{i,j}^t$$
$$\rho_{i,j}^{t+\Delta t} = \rho_{i,j}^t + \Delta t \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^t + \frac{\Delta t^2}{2} \left(\frac{\partial^2 \rho}{\partial t^2}\right)_{i,j}^t$$

Lax-Wendroff Technique - Density

- Second time derivative $\frac{\partial^2 \rho}{\partial t^2}$ can be obtained by differentiating $\frac{\partial \rho}{\partial t} = -\left(\rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y}\right)$ with respect to time $\frac{\partial^2 \rho}{\partial t^2} = -\left(\frac{\partial \rho}{\partial t} \frac{\partial u}{\partial x} + \rho \frac{\partial^2 u}{\partial x \partial t} + \frac{\partial \rho}{\partial t} \frac{\partial v}{\partial y} + \rho \frac{\partial^2 v}{\partial y \partial t} + \frac{\partial u}{\partial t} \frac{\partial \rho}{\partial x} + u \frac{\partial^2 \rho}{\partial x \partial t} + \frac{\partial v}{\partial t} \frac{\partial \rho}{\partial y} + v \frac{\partial^2 \rho}{\partial y \partial t}\right)$ - First time derivatives are computed with spatial
 - derivatives from the governing equations

Lax-Wendroff Technique - Density

Mixed time / spatial derivatives, e.g. $\frac{\partial^2 u}{\partial x \partial t}$, can be obtained by differentiating, e.g. $\frac{\partial u}{\partial t} = -\left(\frac{1}{\rho}\frac{\partial p}{\partial x} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right)$ with respect to x $\frac{\partial^2 u}{\partial x \partial t} = -\left(-\frac{1}{\rho^2}\frac{\partial \rho}{\partial x}\frac{\partial p}{\partial x} + \frac{1}{\rho}\frac{\partial^2 p}{\partial x^2} + \frac{\partial u}{\partial x}\frac{\partial u}{\partial x} + u\frac{\partial^2 u}{\partial x^2} + \frac{\partial v}{\partial x}\frac{\partial u}{\partial y} + v\frac{\partial^2 u}{\partial x \partial y}\right)$ Discretizations of higher-order derivatives, e.g.



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MacCormack Technique - Update

- Velocity and density update with

$$\begin{aligned} u_{i,j}^{t+\Delta t} &= u_{i,j}^{t} + \frac{\Delta t}{2} \left[\left(\frac{\partial u}{\partial t} \right)_{i,j}^{t} + \left(\overline{\frac{\partial u}{\partial t}} \right)_{i,j}^{t+\Delta t} \right] \\ v_{i,j}^{t+\Delta t} &= v_{i,j}^{t} + \frac{\Delta t}{2} \left[\left(\frac{\partial v}{\partial t} \right)_{i,j}^{t} + \left(\overline{\frac{\partial v}{\partial t}} \right)_{i,j}^{t+\Delta t} \right] \\ \rho_{i,j}^{t+\Delta t} &= \rho_{i,j}^{t} + \frac{\Delta t}{2} \left[\left(\frac{\partial \rho}{\partial t} \right)_{i,j}^{t} + \left(\overline{\frac{\partial \rho}{\partial t}} \right)_{i,j}^{t+\Delta t} \right] \end{aligned}$$

 $- (\overline{\frac{\partial}{\partial t}})_{i,j}^{t+\Delta t} \text{ are predicted derivatives at } t + \Delta t \text{ using} \\ \text{predicted values } \overline{\rho}_{i,j}^{t+\Delta t}, \overline{p}_{i,j}^{t+\Delta t}, \overline{u}_{i,j}^{t+\Delta t}, \overline{v}_{i,j}^{t+\Delta t} \text{ at } t + \Delta t \\ \end{array}$

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MacCormack Technique - Prediction

– Prediction

$$\begin{split} \overline{u}_{i,j}^{t+\Delta t} &= u_{i,j}^{t} + \Delta t \left(\frac{\partial u}{\partial t}\right)_{i,j}^{t} \\ &= u_{i,j}^{t} - \Delta t \left(\frac{1}{\rho_{i,j}^{t}} \frac{p_{i+1,j}^{t} - p_{i-1,j}^{t}}{2\Delta x} + u_{i,j}^{t} \frac{u_{i+1,j}^{t} - u_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t} \frac{u_{i,j+1}^{t} - u_{i,j-1}^{t}}{2\Delta y}\right) \\ \overline{v}_{i,j}^{t+\Delta t} &= v_{i,j}^{t} + \Delta t \left(\frac{\partial v}{\partial t}\right)_{i,j}^{t} \\ &= v_{i,j}^{t} - \Delta t \left(\frac{1}{\rho_{i,j}^{t}} \frac{p_{i,j+1}^{t} - p_{i,j-1}^{t}}{2\Delta y} + u_{i,j}^{t} \frac{v_{i+1,j}^{t} - v_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t} \frac{v_{i,j+1}^{t} - v_{i,j-1}^{t}}{2\Delta y}\right) \\ \overline{\rho}_{i,j}^{t+\Delta t} &= \rho_{i,j}^{t} + \Delta t \left(\frac{\partial \rho}{\partial t}\right)_{i,j}^{t} \\ &= \rho_{i,j}^{t} - \Delta t \left(\rho_{i,j}^{t} \frac{u_{i+1,j}^{t} - u_{i-1,j}^{t}}{2\Delta x} + \rho_{i,j}^{t} \frac{v_{i,j+1}^{t} - v_{i,j-1}^{t}}{2\Delta y} + u_{i,j}^{t} \frac{\rho_{i+1,j}^{t} - \rho_{i-1,j}^{t}}{2\Delta x} + v_{i,j}^{t} \frac{\rho_{i,j+1}^{t} - \rho_{i,j-1}^{t}}{2\Delta y}\right) \\ \overline{p}_{i,j}^{t+\Delta t} &= k \left(\frac{\overline{\rho}_{i,j}^{t+\Delta t}}{\rho_{0}} - 1\right) \end{split}$$

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MacCormack Technique – Prediction

Prediction of derivatives

$$\begin{split} \left(\overline{\frac{\partial u}{\partial t}}\right)_{i,j}^{t+\Delta t} &= -\left(\frac{1}{\overline{\rho}_{i,j}^{t+\Delta t}} \frac{\overline{p}_{i+1,j}^{t+\Delta t} - \overline{p}_{i-1,j}^{t+\Delta t}}{2\Delta x} + \overline{u}_{i,j}^{t+\Delta t} \frac{\overline{u}_{i+1,j}^{t+\Delta t} - \overline{u}_{i-1,j}^{t+\Delta t}}{2\Delta x} + \overline{v}_{i,j}^{t+\Delta t} \frac{\overline{u}_{i,j+1}^{t+\Delta t} - \overline{u}_{i,j-1}^{t+\Delta t}}{2\Delta y}\right) \\ \left(\overline{\frac{\partial v}{\partial t}}\right)_{i,j}^{t+\Delta t} &= -\left(\frac{1}{\overline{\rho}_{i,j}^{t+\Delta t}} \frac{\overline{p}_{i,j+1}^{t+\Delta t} - \overline{p}_{i,j-1}^{t+\Delta t}}{2\Delta y} + \overline{u}_{i,j}^{t+\Delta t} \frac{\overline{v}_{i+1,j}^{t+\Delta t} - \overline{v}_{i-1,j}^{t+\Delta t}}{2\Delta x} + \overline{v}_{i,j}^{t+\Delta t} \frac{\overline{v}_{i,j+1}^{t+\Delta t} - \overline{v}_{i,j-1}^{t+\Delta t}}{2\Delta y}\right) \\ \left(\overline{\frac{\partial \rho}{\partial t}}\right)_{i,j}^{t+\Delta t} &= -\left(\overline{\rho}_{i,j}^{t+\Delta t} \frac{\overline{u}_{i+1,j}^{t+\Delta t} - \overline{u}_{i-1,j}^{t+\Delta t}}{2\Delta x} + \overline{\rho}_{i,j}^{t+\Delta t} \frac{\overline{v}_{i,j+1}^{t+\Delta t} - \overline{v}_{i,j-1}^{t+\Delta t}}{2\Delta y}\right) \\ &+ \overline{u}_{i,j}^{t+\Delta t} \frac{\overline{\rho}_{i+1,j}^{t+\Delta t} - \overline{\rho}_{i-1,j}^{t+\Delta t}}{2\Delta x} + \overline{v}_{i,j}^{t+\Delta t} \frac{\overline{\rho}_{i,j+1}^{t+\Delta t} - \overline{\rho}_{i,j-1}^{t+\Delta t}}{2\Delta y}\right) \end{split}$$

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Outline

- Particles vs. grids
- Advection of the velocity field
- Simple grid fluid solvers
- Discussion

Discussion

- Boundary handling
 - Same concepts as for particle fluids
 - Boundary samples with predefined values,
 e.g. mirrored or extrapolated pressure
- Time step
 - Same rules as for particle fluids (CFL number)
 - Velocity times time step should be smaller than cell size
- Viscosity
 - Grid solvers typically suffer from significant artificial viscosity



Discussion

- Staggered grid
 - Velocity and pressure considered at shifted positions
 - Requires interpolations
- Free surface
 - Level sets (initial interface is advected with the flow)
 - Tracer particles (semi-Lagrangian)
- Simulation step
 - Typically subdivided into advection $v_{i,j}^* = v_{i,j}^t \Delta t (v_{i,j}^t \cdot \nabla) v_{i,j}^t$ followed by projection $v_{i,j}^{t+\Delta t} = v_{i,j}^* - \Delta t \frac{1}{\rho_{i,j}^t} \nabla p_{i,j}^t$

Discussion – Grid Solvers in Graphics

Advection

-
$$\boldsymbol{v}_{i,j}^* = \boldsymbol{v}_{i,j}^t - \Delta t (\boldsymbol{v}_{i,j}^t \cdot \nabla) \boldsymbol{v}_{i,j}^t$$

- Typically realized with tracer particles
 - Independent particles are advected with the flow
 - Interpolation of particle velocities from / to cell velocities
 - PIC, FLIP, Stam's stable fluid

Discussion – Grid Solvers in Graphics

– Projection

$$- \boldsymbol{v}_{i,j}^{t+\Delta t} = \boldsymbol{v}_{i,j}^* - \Delta t \frac{1}{\rho_{i,j}^t} \nabla p_{i,j}^t$$

- Pressure is typically computed with a PPE
 - Divergence of predicted velocity as source term
 - No explicit notion of density deviation

Grid-based Fluids



[Carlson et al., SIGGRAPH 2004]

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